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Performance evaluation of an side-stream anaerobic membrane bioreactor: Synthetic and alcoholic beverage industry wastewater

Yan akımlı anaerobik membran biyoreaktör veriminin araştırılması: Sentetik atıksu ve alkollü içki sanayi atıksuyu

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Abstract

The treatment performance of a laboratory-scale anaerobic membrane bioreactor (AnMBR) using high strength wastewater was evaluated. The AnMBR model system consisted of an up-flow anaerobic sludge blanket reactor (UASB) and an ultrafiltration (UF) membrane. Its performance was first examined using molasses based synthetic wastewater at different hydraulic retention times (1-3 days) and organic loading rates (5-15 kg COD/m3.day). As a result of the experimental studies, maximum treatment efficiency with respect to COD reduction (95%) was achieved at 7.5 kg COD/m³.day OLR (COD_{influent}=15.000 mg/L, HRT=2 days) applications. When OLR was increased to 15 kg COD/m³.day, system performance decreased sharply. Similarly, methane gas production decreased by increasing OLR. After then, feed was changed to real wastewater, which was alcoholic beverage industry effluent. At this study, maximum COD removal efficiency of the system and maximum methane gas production was 88% and 74%, respectively.

Keywords: Anaerobic, Membrane, Wastewater, Alcoholic beverage industry

Ör

Yan akımlı anaerobik membran biyoreaktörlerin verimi yüksek kirliliğe sahip atıksular için laboratuvar ölçekli bir sistem kullanılarak irdelenmiştir. Sistem, yukarı akışlı çamur yataklı anaerobik (UASB) reaktör ve ultrafiltrasyon (UF) membran modülünden oluşturulmuştur. Sistemin verimi öncelikle seyreltilmiş melastan hazırlanan sentetik atıksu ile farklı hidrolik alıkonma süreleri (1-3 gün) ve organik yükleme oranlarında (5-15 kg KOİ/m³.day) incelenmiştir. Yapılan deneysel çalışmalar neticesinde, maksimum KOİ giderme verimi (%95) 7.5 kg KOİ/m³.gün organik yükleme değerinde (KOİgirış=15.000 mg/L, HRT=2 gün) elde edilmiştir. Organik yükleme değeri 15 kg KOİ/m³.gün değerine çıkartıldığında sistem performansı aniden düşmüştür. Daha sonra, besleme suyu bir alkollü içki sanayi atıksuyu ile değiştirilerek gerçek atıksu ile çalışmalar yürütülmüştür. Bu çalışmada, maksimum toplam sistem verimi ve metan gazı oluşumu sırasıyla %88 ve %74 olarak belirlenmiştir.

Anahtar kelimeler: Anaerobik, Membran, Atıksu, Alkollü içki sanayi

1 Introduction

Due to the capacity of operation with high organic loads (OLR), the anaerobic membrane bioreactors (AnMBR) are considered to be a superior alternative for the treatment of high strength organic wastewaters [1],[2]. An AnMBR can be simply defined as a biological treatment process operated without oxygen and using a membrane to provide solid-liquid separation [2].

The applicable organic load changes depending on the wastewater properties, operational conditions, and the design of the reactors. Lin et al. (2013) reported that most studies regarding AnMBR applied lower than 10 kg COD/m³.d [2]. He et al. (2005) reported that COD removal efficiencies higher than 90% and 80% were obtained at organic loading rates of 2.0 kg/m³.d and 2.0-4.5 kg/m³.d, respectively for high strength food wastewater [3]. In another study, OLR of 20 kg/m3.d, 8 kg/m³.d and 6-8 kg/m³.d was applied for synthetic wastewater, for the vegetable processing industry (sauerkraut brine) wastewater and for the wastewater from an animal slaughterhouse, respectively. COD removal efficiencies above 90% were obtained in all applications [4]. Bohdziewicz et al. (2008) found the highest efficiency in terms of COD removal 90% at hydraulic retention time (HRT) of 2 days and OLR of 2.5 kg COD/m3.d for landfill leachate treatment by an anaerobic submerged membrane bioreactor [5]. A slaughterhouse that used AnMBR to treat wastewater achieved about 94% average COD removal efficiency at OLRs between 4.37 and 13.27 kg COD/m³.d [6].

Although there are several studies about AnMBR in the literature, as reported by Dereli et al., there is still a large knowledge gap for the design and operation of full-scale AnMBRs [7]. The purpose of the present study is to evaluate the performance of an anaerobic side-stream membrane bioreactor under different operational conditions for high strength wastewater (i.e. synthetic wastewater and alcoholic beverage industry effluent) for optimum design conditions and for operating full scale AnMBR systems.

2 Materials and methods

2.1 Laboratory scale AnMBR system

Experimental studies were carried out using a side-stream (external) AnMBR consisting of an anaerobic reactor and an ultrafiltration (UF) unit (Figure 1). The side-stream configuration was selected due to their some advantages such as easier membrane replacement and fouling control.

The feeding tank and anaerobic reactor are made of stainless steel. The anaerobic reactor was designed as an up-flow anaerobic sludge blanket (UASB) reactor. There is no mixing device and gas/liquid/solid separation system in the anaerobic

reactor. It was operated under mesophilic ($36\pm1\,^{\circ}$ C) conditions and the temperature was kept constant by circulating hot water through the reactor jacket. With a total volume of 10 liters, the anaerobic reactor was equipped with inlet and outlet valves, sampling valves, and gas and sludge outlet valves. Wastewater was introduced to the anaerobic reactor at the bottom and effluent was withdrawn from the top of the reactor and pumped to the UF unit.

A hollow fiber polysulfone membrane in Pall's Microza module (SLP-1053) was used as the membrane module following-anaerobic reactor. The molecular weight cut-off and surface area of the membrane was 10 kDa and 0.1 m², respectively. A peristaltic pump was used to pump the wastewater to the membrane system. Inlet and outlet pressure was measured using pressure measurement devices attached to the module. The inlet pressure was kept constant at 1.5 ± 0.2 bars during the experiments. The maximum wash and backwash pressures for the UF membrane were 1.7 and 2.5 bar, respectively.

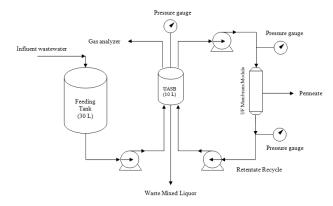


Figure 1: The flow scheme of the model system.

2.2 Wastewater characteristics

After the start-up phase, high strength synthetic wastewater consisting of the diluted molasses was first used. The composition of synthetic wastewater is given in Table 1. The COD concentration range of some high strength industrial wastewaters including yeast factory effluent, sugar industry effluent, and fermentation industry effluent changes between 8.000-30.000 mg/L [8]-[11]. Therefore, COD concentrations range of the synthetic wastewater was selected considering the above COD concentration range of high strength industrial wastewaters.

Following the study with synthetic wastewater, raw alcoholic beverage industry effluent was fed to the model reactor. The COD concentration of the wastewater used in this study was about 5600 ± 800 mg/L and pH of the wastewater ranged between 6.1-10.8.

2.3 Analytical procedure

During the experimental study, analyses of pH, total chemical oxygen demand (COD), alkalinity, volatile fatty acids, total solids (TS), total volatile solids (TVS), total suspended solids (TSS), and volatile suspended solids (VSS) were carried out according to Standard Methods [12]. The pH was measured using the WTW model 340i multi analyzer. The composition of the biogas (CH₄ and CO₂) was measured using a Dräger X AM 7000 multi gas measurement device. Total biogas and methane

production volume were also determined by the liquid displacement methods.

Table 1: The composition of the synthetic wastewater

Parameter	Range	
COD, mg/L	15.000-20.000	
TS, mg/L	18.800±3.300	
TVS, mg/L	15.700±2950	
TSS, mg/L	250±125	
TVS, mg/L	85±70	
Total nitrogen, mg/L	26±1	
Phosphate, mg/L	1.5±0.9	
рН	7±2	

2.4 Start-up phase

The anaerobic reactor was inoculated by adding sludge produced in the anaerobic reactors of PAKMAYA Baker's Yeast Company (Izmir, Turkey) Wastewater Treatment Plant. The model reactor was operated at 5 days HRT and at an OLR of 0.4 kg/m³.d with an influent COD concentration of 2000 mg/L at the start-up phase. The system has reach to steady-state conditions after 30 days continuous operation.

2.5 Operational conditions

After the reactor start-up stage, the influence of HRT and OLR were investigated. In this scope, four different operational conditions given in Table 2 were applied during the studies with synthetic wastewater. System performance was evaluated at three hydraulic retention times (3, 2, and 1 days) and two influent COD concentrations (15.000-20.000 mg/L). There was about two weeks between tested phases for reaching steady-state conditions and after then the model reactor was operated about one month at each phase.

Table 2: Applied operational conditions.

		Influent COD Concentration, mg/L	Hydraulic Retention Time (HRT), day	Organic Loading Rate (OLR), kg COD/m³*day
Synthetic Wastewater	Phase I	15000	3	5
	Phase II	15000	2	7.5
	Phase III	15000	1	15
	Phase IV	20000	2	10
Alcoholic Beverage Wastewater		5600±800	2	2.4-3.2

Following the studies with synthetic wastewater, alcoholic beverage industry effluent was fed to the model reactor for about a month. The operational conditions were adjusted considering the optimum conditions which had been determined in previous study carried out with synthetic wastewater. Since the maximum treatment efficiency was achieved at 2 days of HRT, the hydraulic retention time was kept constant at 2 days (Q=5 L/day) during the synthetic

wastewater experiments. The organic loading rate was between 2.4-3.2 kg COD m³ per day depending on the influent COD concentrations (Table 2).

3 Results and discussion

3.1 Synthetic wastewater

The pH, alkalinity and VFA/Alkalinity ratio changes in the anaerobic reactor effluent were monitored regularly. There was no significant pH fluctuation and the average pH of the effluent was 6.9. The alkalinity and VFA in the anaerobic reactor effluent was measured between 2800-4400 mg CaCO₃/L and 200-2500 mg/L, respectively. A decrease in the alkalinity and an increase in the VFA with increasing OLR were observed. The VFA and alkalinity, separately, are not good indicators for evaluating the process stability of the anaerobic reactor, since total alkalinity reflect both levels of VFA and bicarbonate, and unstable conditions increased VFA, and reduced the bicarbonate, resulting in constant total alkalinity [13]. Thus, the ratio of VFA to alkalinity is the best option to monitor process stability in anaerobic systems. As reported by Zhao and Viraraghavan (2004) if VFA/Alkalinity ratio exceeds 0.8, the inhibition of methanogens occurs and the process failure is apparent [14]. In this study, VFA/Alkalinity ratio varied between 0.1 and 1.02. At higher OLR applications (Phase III and IV), ratios above 0.8 were measured. In order to protect the methanogenic and acetogenic populations from VFAs accumulation, a certain amount of alkalinity was added regularly.

Maximum COD removal efficiencies for the anaerobic reactor, the UF membrane unit, and the overall system (AnMBR) are shown in Figure 2. In the anaerobic reactor, maximum COD removals of 55%, 80%, 63% and 61% were obtained for OLRs of 5 kg COD/m3.d (Phase I), 7.5 kg COD/m3.d (Phase II), 15 kg COD/m3.d (Phase III), and 10 kg COD/m3.d (Phase IV), respectively. Although influent COD concentrations of Phase I-II and III are the same, decreasing HRT was applied for these experiments. As seen from the Figure 2, organic material removal efficiencies of the anaerobic reactor decrease with decreasing HRT and increasing OLR. Skouteris et al. (2012) indicated that, when the organic loading rate increases, the risk of a deteriorated performance due to volatile fatty acids (VFAs) accumulation may occur, and lower COD removal efficiencies are achieved due to the inhibition of microbial activity [15]. As indicated above, increase in VFA with increasing OLR was also observed in this study.

The COD removal efficiencies of the UF membrane decreased from 75% to 46% as operation continued. In MBR systems, COD is removed by both physical and biological mechanisms. Amri (2010) indicated that although the biological COD removal increases in time, the COD removal by the membrane decreases in time because of the age of the membrane and membrane fouling [16]. However, some researchers pointed out that the fouling layer at the membrane surface provides extra filtration activity and removal efficiency increases [17]. The other reason for the decrease in membrane efficiency may be the increase in the organic matter concentration of influent wastewater. Since influent COD concentrations increased throughout the experimental study, organic material content of the anaerobic reactor effluent also increased over time.

In terms of overall system (AnMBR) performance, maximum COD removal efficiencies of 85%, 95%, 88%, and 79% were obtained at 5 kg COD/m 3 .d (COD_{influent}=15.000 mg/L,

HRT=3 day), 7.5 kg COD/m³.d (COD_{influent}=15.000 mg/L, HRT=2 day), 15 kg COD/m³.d (COD_{influent}=15.000 mg/L, HRT=1 day) and 10 kg COD/m³.d (COD_{influent}=20.000 mg/L, HRT=2 day) of OLRs, respectively. The lowest efficiency of 79% was obtained at the highest influent COD concentration feeding (Phase IV). In a study carried out with synthetic wastewater consisted of molasses 78-81% COD removal were obtained at 14.9-5.6 kg COD/m³.d of OLR and 16-32 h of HRT [18].

The decrease in HRT negatively influenced the COD removal in the AnMBR. However, Stuckey (2012) reported that some researchers operated such systems at HRT as low as 4 h and 97% COD removal could be achieved at temperatures down to $13 \, ^{\circ}$ C [19].

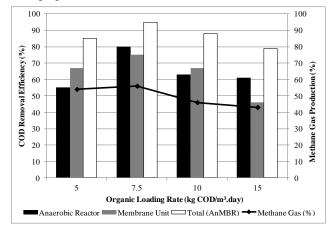


Figure 2: Performance of the system vs. organic loading rates for synthetic wastewater.

Average methane gas percentage of the total produced biogas during Phase I (5 kg COD/m³.d), Phase II (7.5 kg COD/m³.d), Phase III (15 kg COD/m³.d), and Phase IV (10 kg COD/m³.d) were observed as 54%, 56%, 46%, and 43%, respectively (Figure 2). It was observed that methane content of the total produced biogas decreased with an increase in the OLR and with a decrease in the HRT. Since methane production is the key parameter for an efficient anaerobic biodegradation, lower methane contents represented that high organic loading and low hydraulic retention time negatively affected the performance of the AnMBR system.

During the experimental studies, average total and volatile solids concentrations in the anaerobic reactor effluent were 7.000 mg/L and 2.660 mg/L, respectively. UF did not indicate any effective TS and TVS removals with respective maximum efficiencies of 25% TS and 38% and with respective average efficiencies of 15% and 31%. The UF membrane system can produce high quality water, free of suspended solids, colloidal material, and bacteria [20]. As expected, high total suspended solids (97% average) and volatile suspended solids (93% average) removals were obtained with the UF membrane system in this study. Figure 3 shows a noticeable elimination of suspended solids by the change of the permeate turbidity.

3.2 Alcoholic beverage wastewater

Although the influent pH changed in a wide range (i.e. 6.1-10.8), pH values in the effluents of the anaerobic reactor and membrane unit, which were in the range of 7.1-7.6 and 7.3-7.8, respectively, were almost constant. The average alkalinity and volatile fatty acids in the anaerobic reactor effluent was 1400 mg/L and 210 mg/L, respectively. Thus,

VFA/Alkalinity ratio was about 0.15 during the operational period.

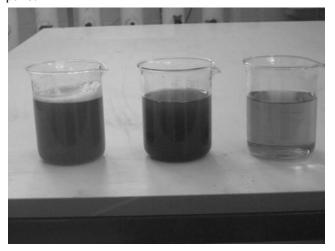


Figure 3: Feeding wastewater (left), anaerobic reactor effluent (middle), permeate (right).

Total COD removal performance of the model reactor for alcoholic beverage industry effluent was illustrated in Figure 4. The COD concentrations of raw influent were 5600±800 mg/L, and that of AnMBR effluent remained 800 mg/L at steady-state conditions. COD removal efficiencies of the model reactor changed from 69 to 88%, while the average was 82%. Torres et al. (2011) operated a lab-scale AnMBR operated with external membrane modules containing inside/out tubular membranes and higher than 97% COD removal was obtained in an OLR range up to 12 kg COD/m³.d [21].

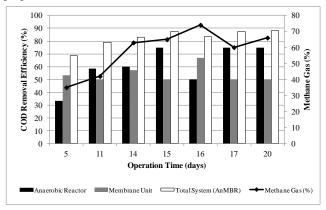


Figure 4: Performance of the system for alcoholic beverage industry effluent.

A higher methane gas percentage (74%) was obtained in studies with beverage wastewater, compared to that of obtained with synthetic wastewater treatment. Wastewater from beverage production facilities contains easily biodegradable organic compounds (BOD $_5$ /COD= \sim 0.5) and treatment of this type of wastewater usually comprises of physical pre-treatment for removal of suspended matter followed by biological treatment, either aerobic or anaerobic [21]. Matošić et al. (2009) compared the performances of an aerobic MBR and a conventional activated sludge process treating beverage industry effluent [22]. Results of the study indicated that, MBR successfully removed the pollutants in terms of COD, BOD, and TOC from the wastewater with an

efficiency of over 90%. However, it must be kept in mind that

aerobic systems consume huge amount of energy while the anaerobic processes produce methane, which is a valuable energy source.

4 Conclusions

Treatment studies of both synthetic and real high strength wastewater were carried out using a laboratory-scale side-stream anaerobic membrane bioreactor (AnMBR), consisting of an up-flow anaerobic sludge blanket (UASB) reactor and an ultrafiltration (UF) membrane. Results of the study with synthetic wastewater indicated that, maximum COD efficiency (95%) was achieved at an OLR of 7.5 kg COD/m³.day. When OLR increased two-fold, system performance decreased sharply. Similarly, methane gas production decreased by increasing OLR. On the other hand, results of the study with rawalcoholic beverage industry effluent, maximum 88% COD removal was obtained. As a conclusion, it was found that, anaerobic membrane bioreactors can be applied to treat high strength organic wastewaters. AnMBR is a good alternative for treating these types of wastewaters providing high quality effluent.

5 Acknowledgement

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